



Real-Time Optimization
Methods and Applications

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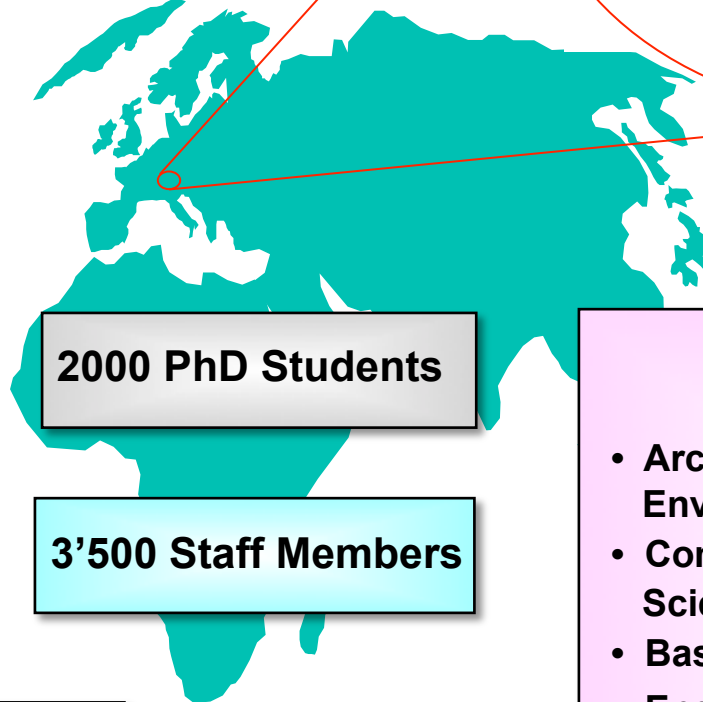
ÉCOLE POLYTECHNIQUE
FÉDÉRALE DE LAUSANNE



8000 B/M Students

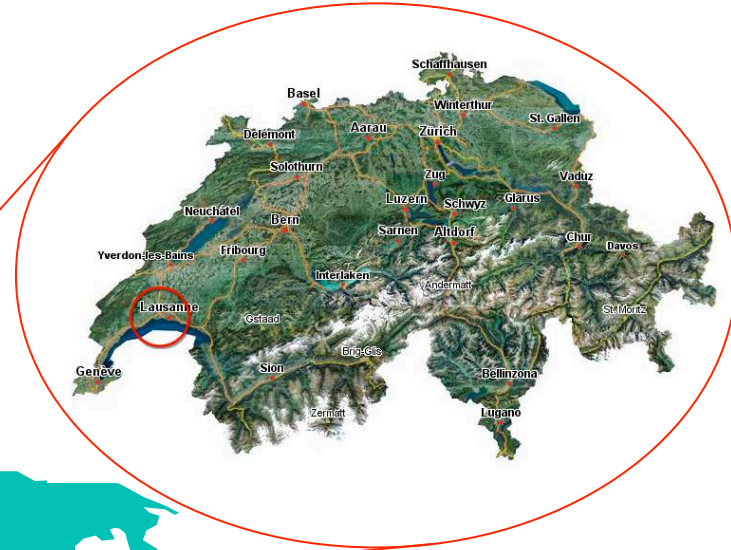
350 Professors

Global Budget
850 Mios CHF



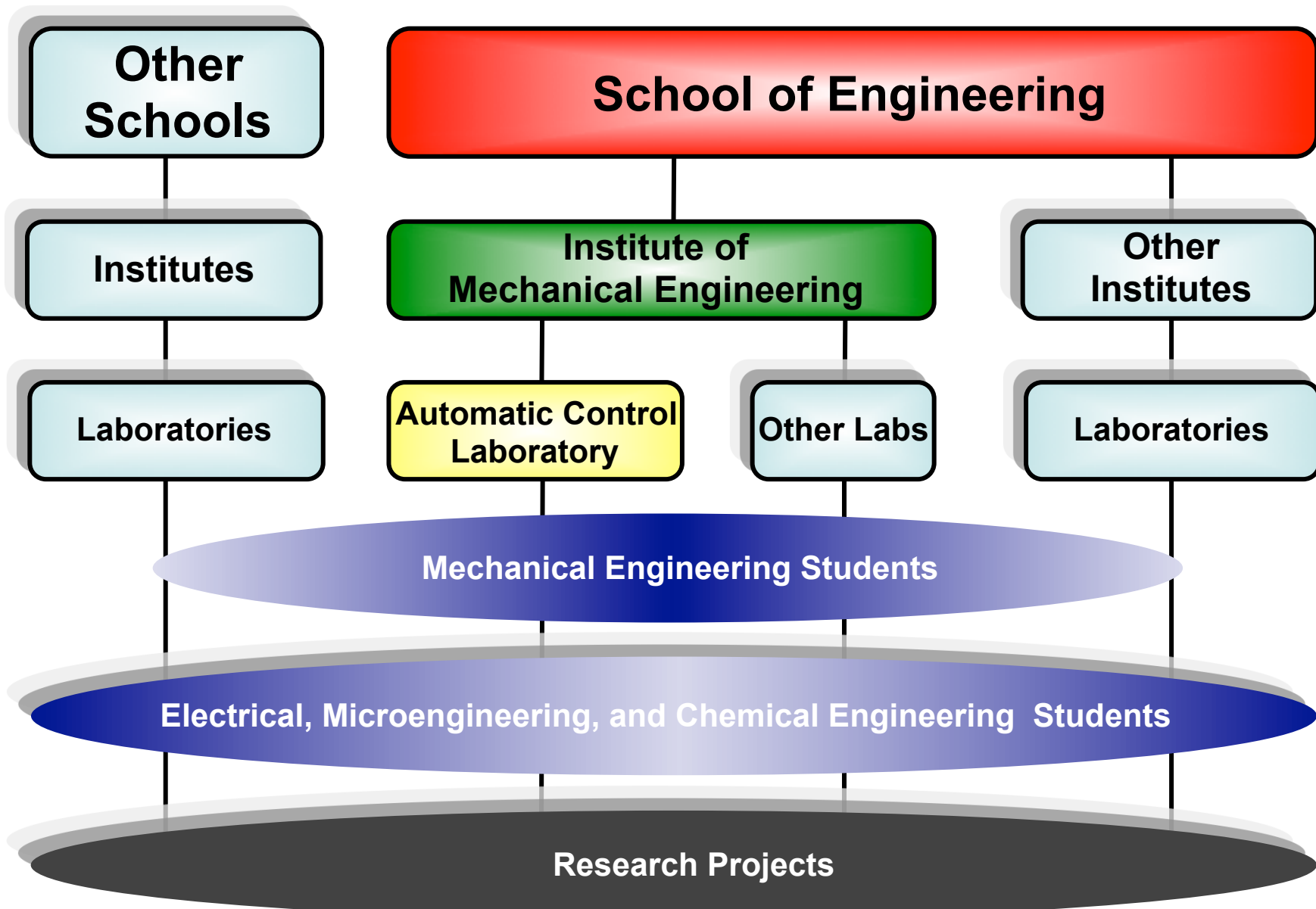
2000 PhD Students

3'500 Staff Members



5 Schools

- Architecture, Civil & Environmental Engineering
- Computer & Communication Sciences
- Basic Sciences
- Engineering
- Life Sciences



Real-Time Optimization

Methods and Applications

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Madrid, April 2016

Outline

1. Real-time optimization

- Use of real-time measurements to improve process operation in the presence of uncertainty
- What to measure and what to adapt?

2. Three RTO schemes

- Update **model parameters** and repeat numerical optimization
- Modify **cost** and **constraints** and repeat numerical optimization
- Optimization via **feedback control**

3. Two experimental case studies

- Solid oxide fuel cell stack
- Batch polymerization reactor



Optimization of Process Operation

1. Features of industrial processes

- Complexity
 - Presence of disturbances
- } → uncertainty

2. Operational objectives

- **Feasibility**: respect operational and safety constraints
- **Optimality**: minimize energy, maximize efficiency, maximize productivity

3. Performance improvement

- On the basis of a model via **numerical optimization**
 - ✓ Difficult in practice because of model inaccuracies, disturbances
- Use measurements → **real-time optimization**
 - ✓ What to measure, what to adapt?

Optimization of a Continuous Plant

Optimize the **steady-state performance** of a (dynamic) process while satisfying a number of operating constraints

Plant

$$\begin{aligned} \min_{\mathbf{u}} \quad & \phi_p(\mathbf{u}, \mathbf{y}_p) \\ \text{s. t.} \quad & \mathbf{g}_p(\mathbf{u}, \mathbf{y}_p) \leq \mathbf{0} \end{aligned}$$

Inputs \mathbf{u} ?
(set points)



Plant
Outputs \mathbf{y}_p

Model-based Numerical Optimization

$$\begin{aligned} & \mathbf{F}(\mathbf{u}, \mathbf{y}, \boldsymbol{\theta}) = \mathbf{0} \\ \min_{\mathbf{u}} \quad & \Phi(\mathbf{u}, \boldsymbol{\theta}) := \phi(\mathbf{u}, \mathbf{y}) \\ \text{s. t.} \quad & \mathbf{G}(\mathbf{u}, \boldsymbol{\theta}) := \mathbf{g}(\mathbf{u}, \mathbf{y}) \leq \mathbf{0} \end{aligned}$$

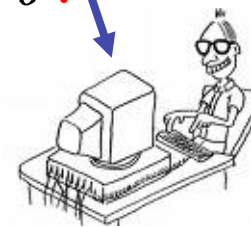
StOP

NLP

Model

Parameters $\boldsymbol{\theta}$?

Inputs \mathbf{u} ?
(set points)



Predicted
Outputs \mathbf{y}

Optimization of a Batch Plant



Batch reactor with finite terminal time

Input parameterization

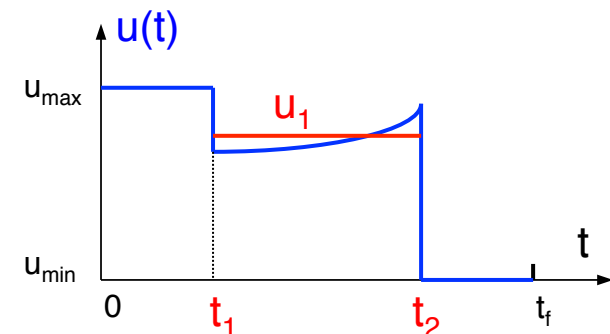
$$u[0, t_f] = U(\pi)$$



Batch reactor viewed as a static map

Repetitive Dynamic Process

$$\begin{aligned} \min_{u[0, t_f]} \quad & \Phi := \phi(\mathbf{x}(t_f)) \\ \text{s. t.} \quad & \dot{\mathbf{x}} = \mathbf{F}(\mathbf{x}, \mathbf{u}, \theta) \quad \mathbf{x}(0) = \mathbf{x}_0 \\ & \mathbf{S}(\mathbf{x}, \mathbf{u}) \leq \mathbf{0} \\ & \mathbf{T}(\mathbf{x}(t_f)) \leq \mathbf{0} \end{aligned} \quad \text{DyOP}$$



$$\begin{aligned} \min_{\pi} \quad & \Phi(\pi, \theta) \\ \text{s. t.} \quad & \mathbf{G}(\pi, \theta) \leq \mathbf{0} \end{aligned} \quad \begin{array}{l} \text{StOP} \\ \text{NLP} \end{array}$$

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2. Three RTO schemes
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3. Experimental case study
 - Solid oxide fuel cell stack
 - Batch polymerization reactor



Three Approaches for Static RTO

What to measure and what to adapt?

Optimization in the presence
of **Uncertainty**

$$\mathbf{u}^* \in \arg \min_{\mathbf{u}} \Phi(\mathbf{u}, \boldsymbol{\theta})$$

s.t. $\mathbf{G}(\mathbf{u}, \boldsymbol{\theta}) \leq \mathbf{0}$

input update: $\delta \mathbf{u}$

parameter update: $\delta \boldsymbol{\theta}$

cost & constraint update: $\delta \Phi, \delta \mathbf{G}$

No Measurement:
Robust Optimization

Measurements:
Adaptive Optimization

1

2

3

Measure
Outputs
and adapt
Model Parameters

Measure/Estimate
KKT elements
and adapt
Cost & Constraints

Measure/Estimate
KKT elements
and adapt
Inputs

- *two-step approach*
(repeated identification
and optimization)

- bias update
- gradient correction
- *modifier adaptation* © LA

- *self-optimizing control*
- *NCO tracking* © LA
- *extremum-seeking control*

Explicit methods

Implicit method

1. Adaptation of Model Parameters

Two-step approach

Parameter Identification Problem

$$\theta_k^* \in \arg \min_{\theta} J_k^{\text{id}}$$

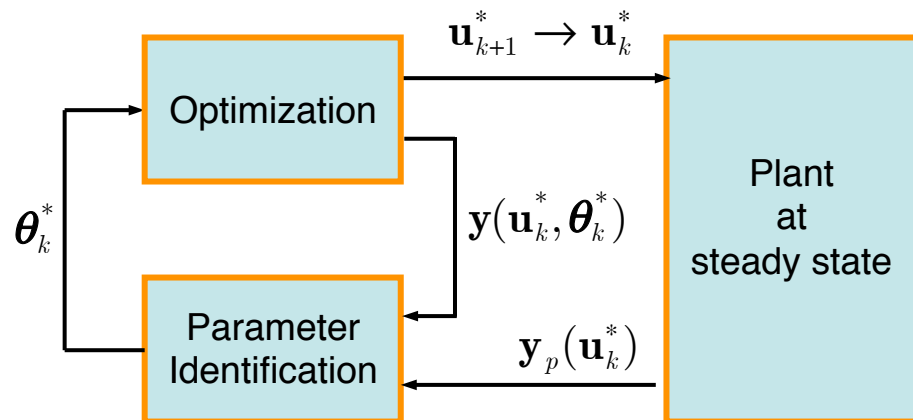
$$J_k^{\text{id}} = \left[\mathbf{y}_p(\mathbf{u}_k^*) - \mathbf{y}(\mathbf{u}_k^*, \theta) \right]^T \mathbf{Q} \left[\mathbf{y}_p(\mathbf{u}_k^*) - \mathbf{y}(\mathbf{u}_k^*, \theta) \right]$$

Optimization Problem

$$\mathbf{u}_{k+1}^* \in \arg \min_{\mathbf{u}} \phi(\mathbf{u}, \mathbf{y}(\mathbf{u}, \theta_k^*))$$

$$\text{s.t. } \mathbf{g}(\mathbf{u}, \mathbf{y}(\mathbf{u}, \theta_k^*)) \leq \mathbf{0}$$

$$\mathbf{u}^L \leq \mathbf{u} \leq \mathbf{u}^U$$

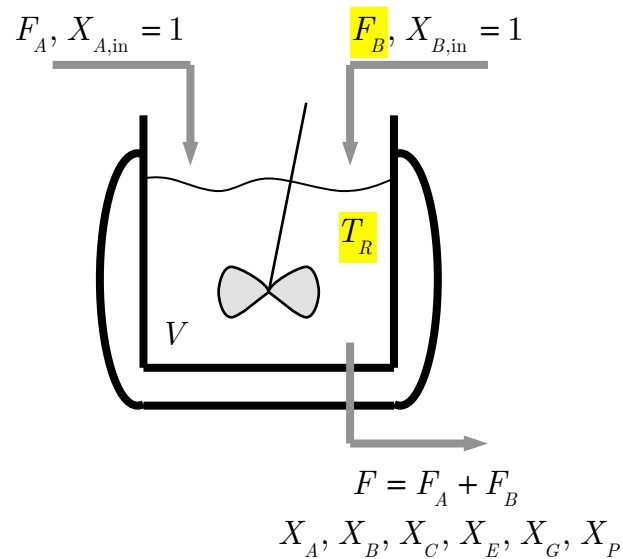


Current Industrial Practice
for tracking the changing optimum
in the presence of disturbances

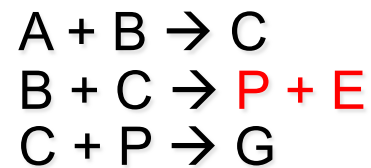
T.E. Marlin, A.N. Hrymak. Real-Time Operations Optimization of Continuous Processes,
AIChE Symposium Series - CPC-V, 93, 156-164, 1997

Example of Plant-Model Mismatch

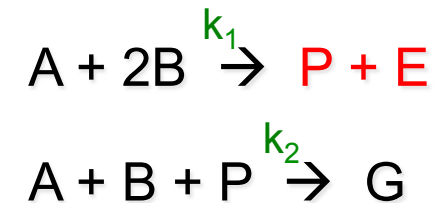
Williams-Otto reactor



3-reaction system



2-reaction model

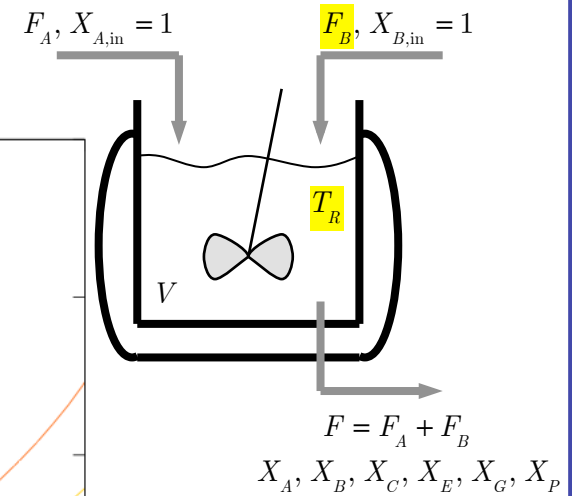
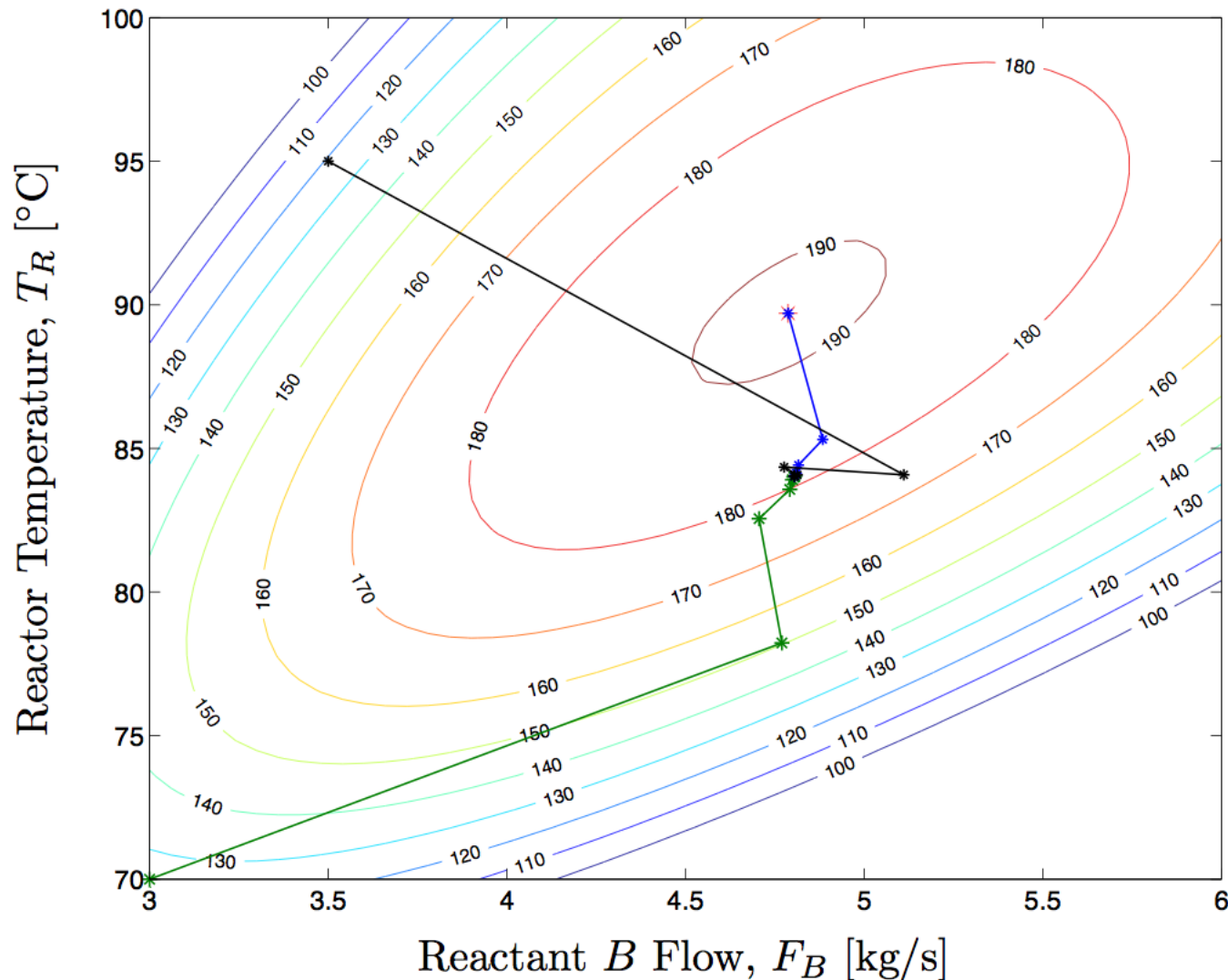


Objective: maximize productivity

Model

- 4th-order model
- 2 inputs
- 2 adjustable parameters (k_{10}, k_{20})

Two-step Approach With structurally incorrect model



Williams-Otto Reactor

- 4th-order model
- 2 inputs
- 2 adjustable par.

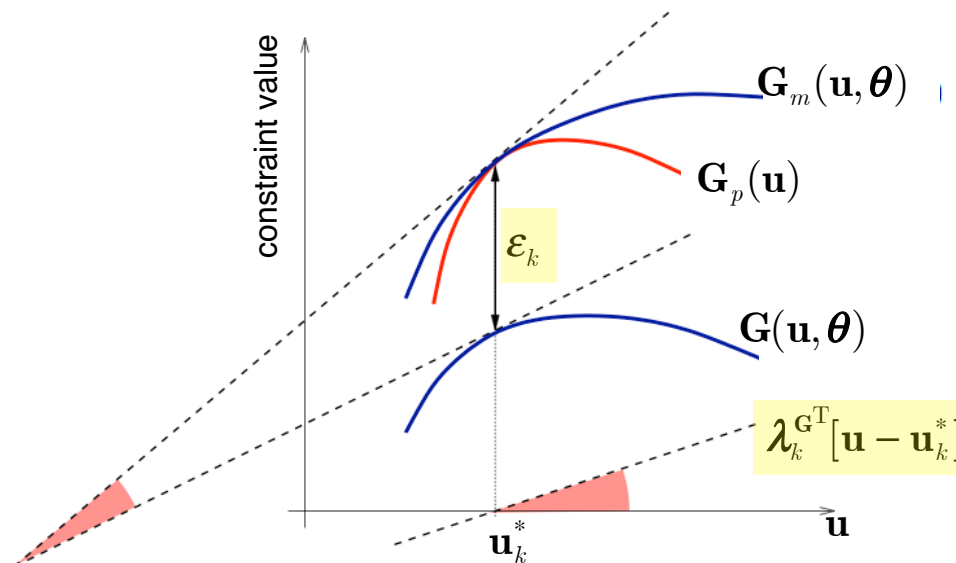
Does not
converge to plant
optimum

2. Adaptation of Cost & Constraints Input-affine correction to the model

Modified Optimization Problem

$$\begin{aligned} \mathbf{u}_{k+1}^* \in \arg \min_{\mathbf{u}} \quad & \Phi_m(\mathbf{u}, \boldsymbol{\theta}) := \Phi(\mathbf{u}, \boldsymbol{\theta}) + \lambda_k^{\Phi T} [\mathbf{u} - \mathbf{u}_k^*] \\ \text{s.t.} \quad & \mathbf{G}_m(\mathbf{u}, \boldsymbol{\theta}) := \mathbf{G}(\mathbf{u}, \boldsymbol{\theta}) + \boldsymbol{\varepsilon}_k + \lambda_k^{G T} [\mathbf{u} - \mathbf{u}_k^*] \leq 0 \\ & \mathbf{u}^L \leq \mathbf{u} \leq \mathbf{u}^U \end{aligned}$$

Affine corrections of cost and constraint functions.
The modified problem satisfies the first-order optimality conditions of the plant



$$\lambda_k^G = \frac{\partial \mathbf{G}_p}{\partial \mathbf{u}}(\mathbf{u}_k^*) - \frac{\partial \mathbf{G}}{\partial \mathbf{u}}(\mathbf{u}_k^*, \boldsymbol{\theta})$$

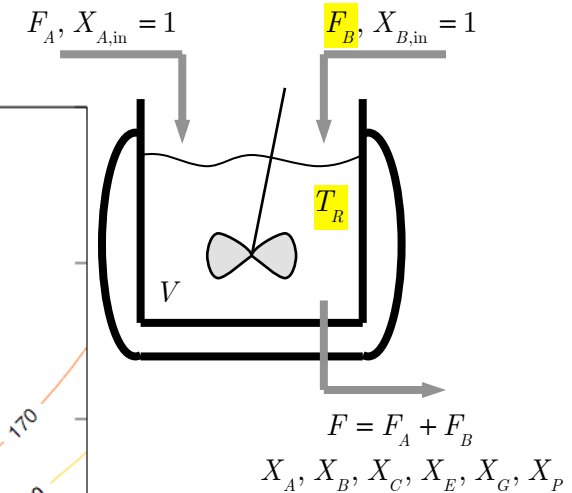
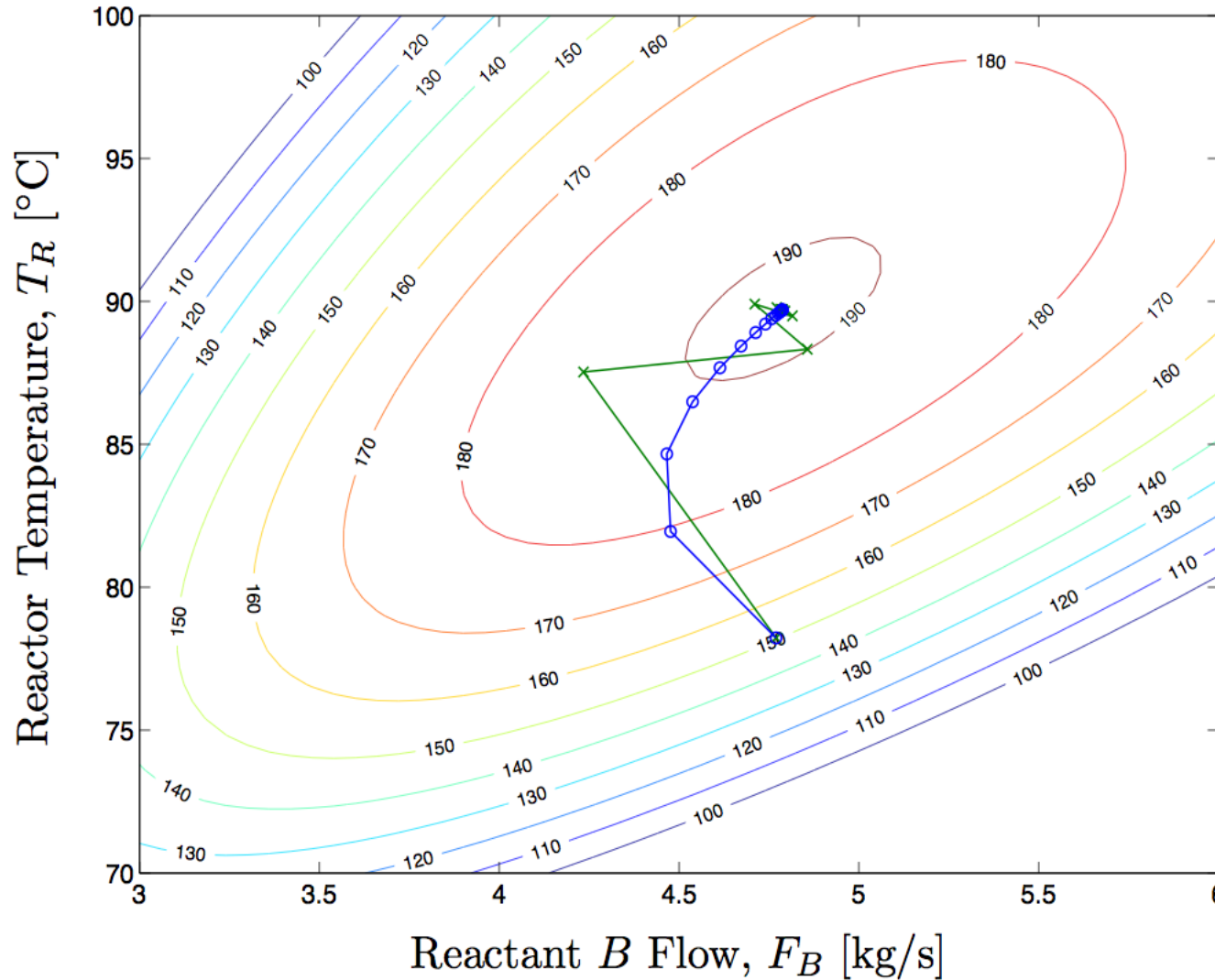
plant gradients

P.D. Roberts, On an Algorithm for Combined System Optimization and Parameter Estimation, *Automatica*, **17**, 199–209, 1981

A. Marchetti, Modifier-Adaptation Methodology for Real-Time Optimization, *I&EC Research*, **48**, 6022-6033, 2009

Example Revisited

Modifier adaptation



Williams-Otto Reactor

- 4th-order model
- 2 inputs
- 2 adjustable par.

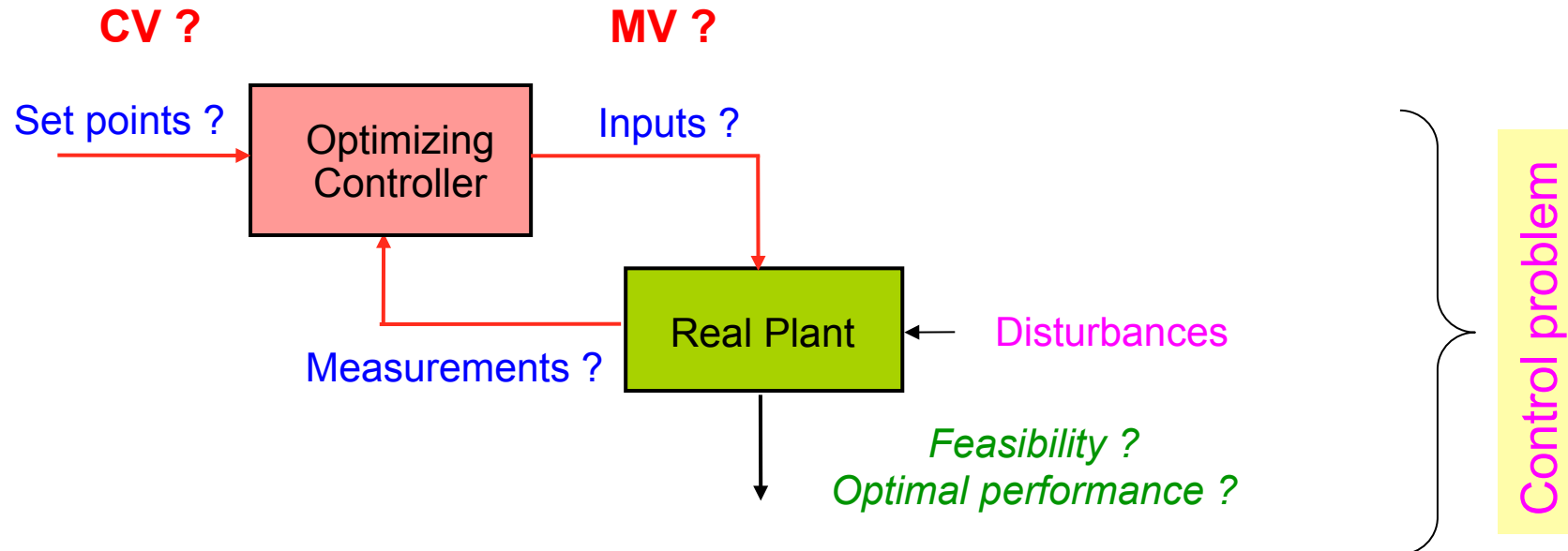
Converges to plant optimum

Requires estimation of experimental gradient

3. Direct Adaptation of Inputs

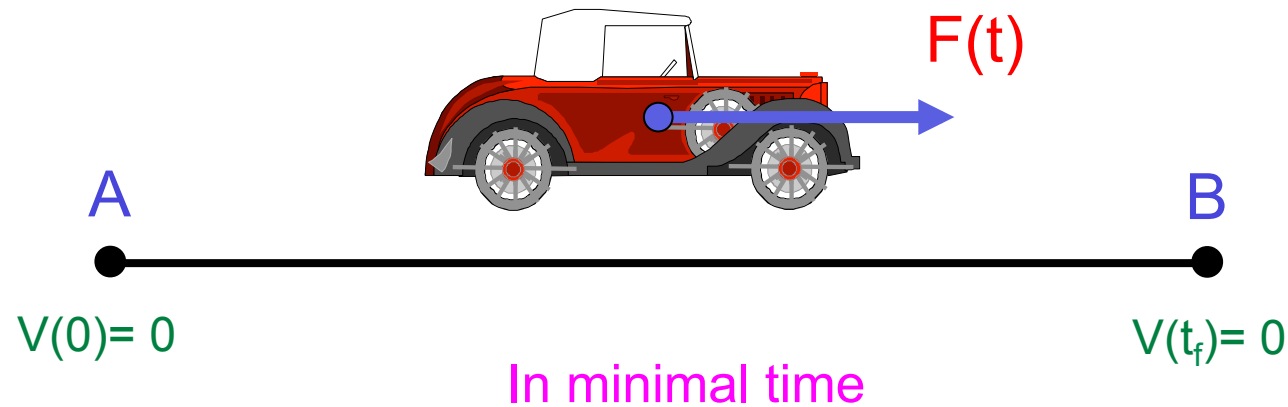
NCO tracking © LA

- Transform the optimization problem into a control problem
- Which setpoints to track for optimality?
 - The **optimality conditions** (active constraints, gradients)
 - Requires appropriate measurements



B. Srinivasan and D. Bonvin, Real-Time Optimization of Batch Processes by Tracking the Necessary Conditions of Optimality, *I&EC Research*, 46, 492-504 2007.

Example Minimum-time Problem

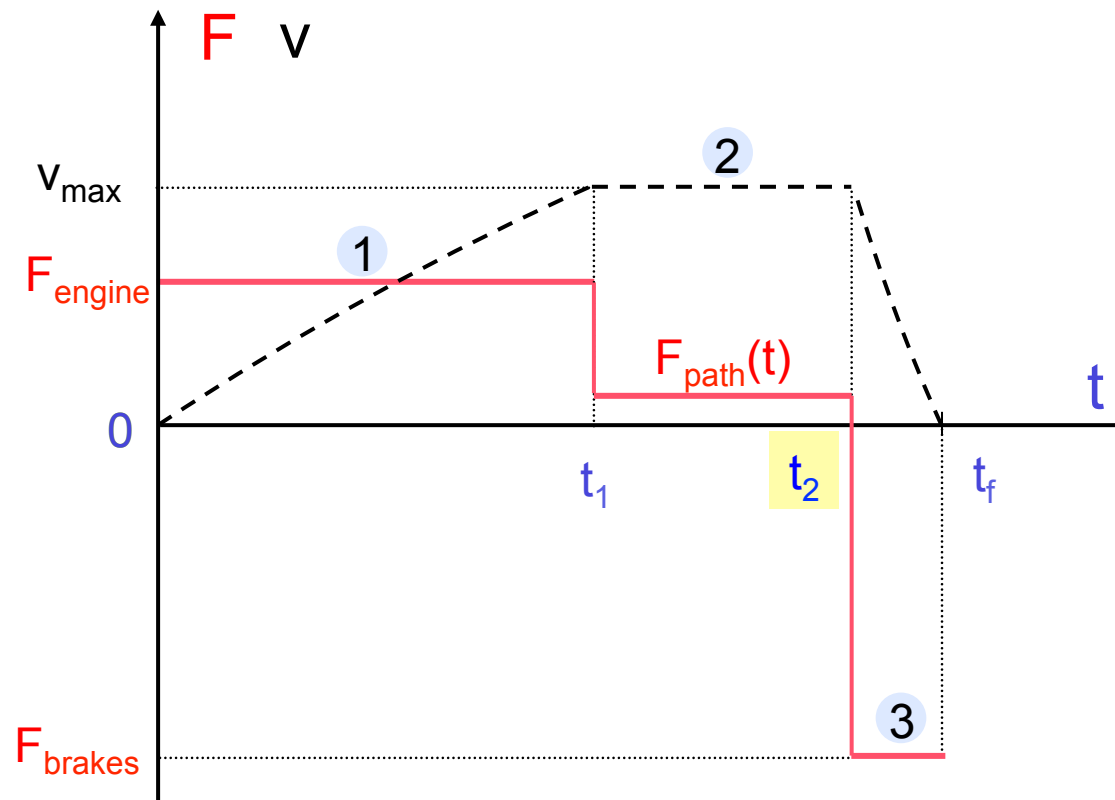


Path constraints: $F_{\text{brakes}} \leq F(t) \leq F_{\text{engine}}$ $v(t) \leq v_{\text{max}}$

Terminal constraints: $v(t_f) = 0$ $x(t_f) \geq x_{\text{des}}$

Problem: Find the **force** $F(t)$ that minimizes t_f

Optimal Trajectories



Faster Car



Path constraints:

$$F_{\text{brakes}} \leq F(t) \leq F_{\text{engine}}$$

$$v(t) \leq v_{\text{max}}$$

Terminal constraints:

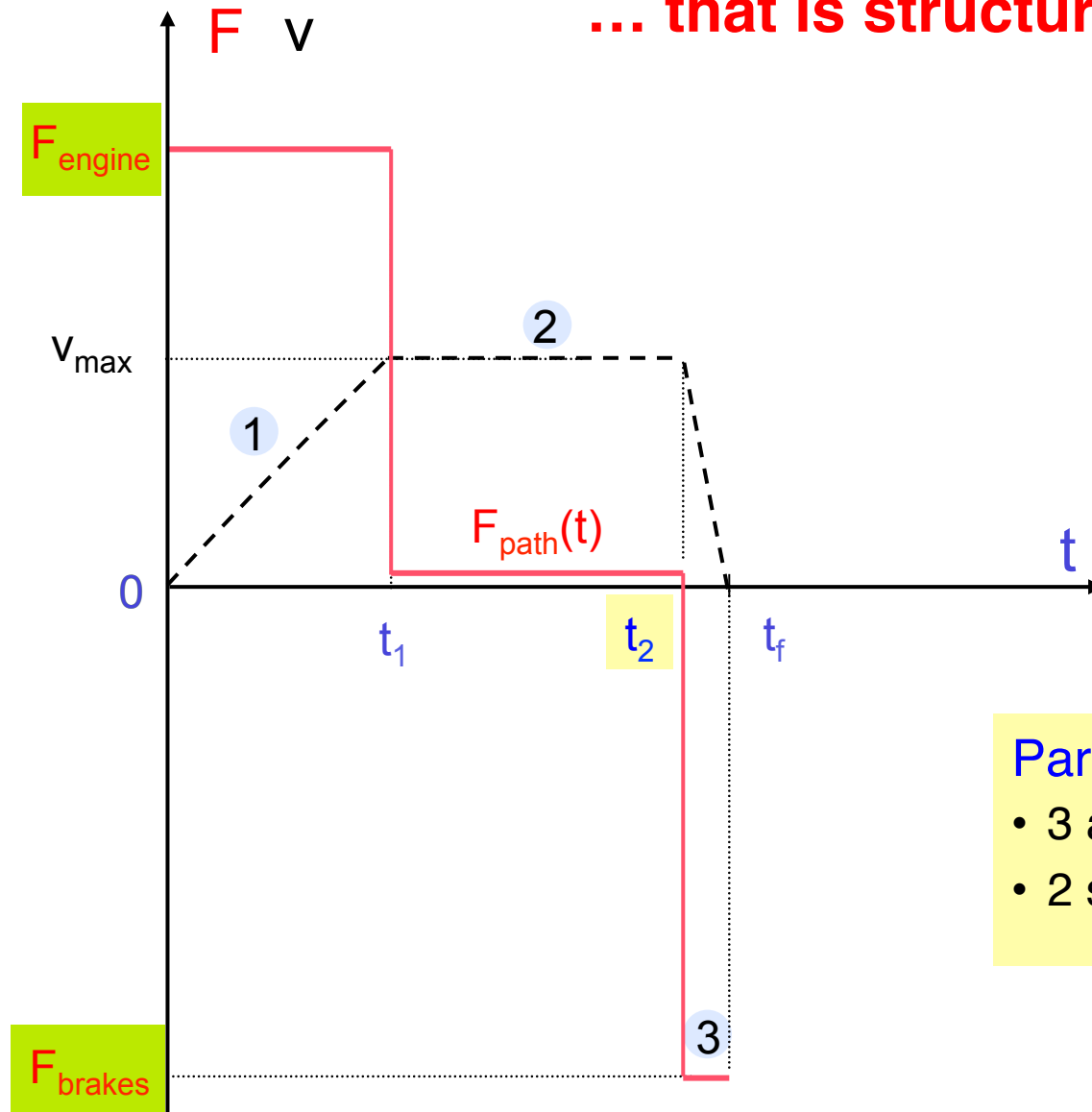
$$v(t_f) = 0$$

$$x(t_f) \geq x_{\text{des}}$$

Problem: Find the **force** $F(t)$ that minimizes t_f

Different Solution

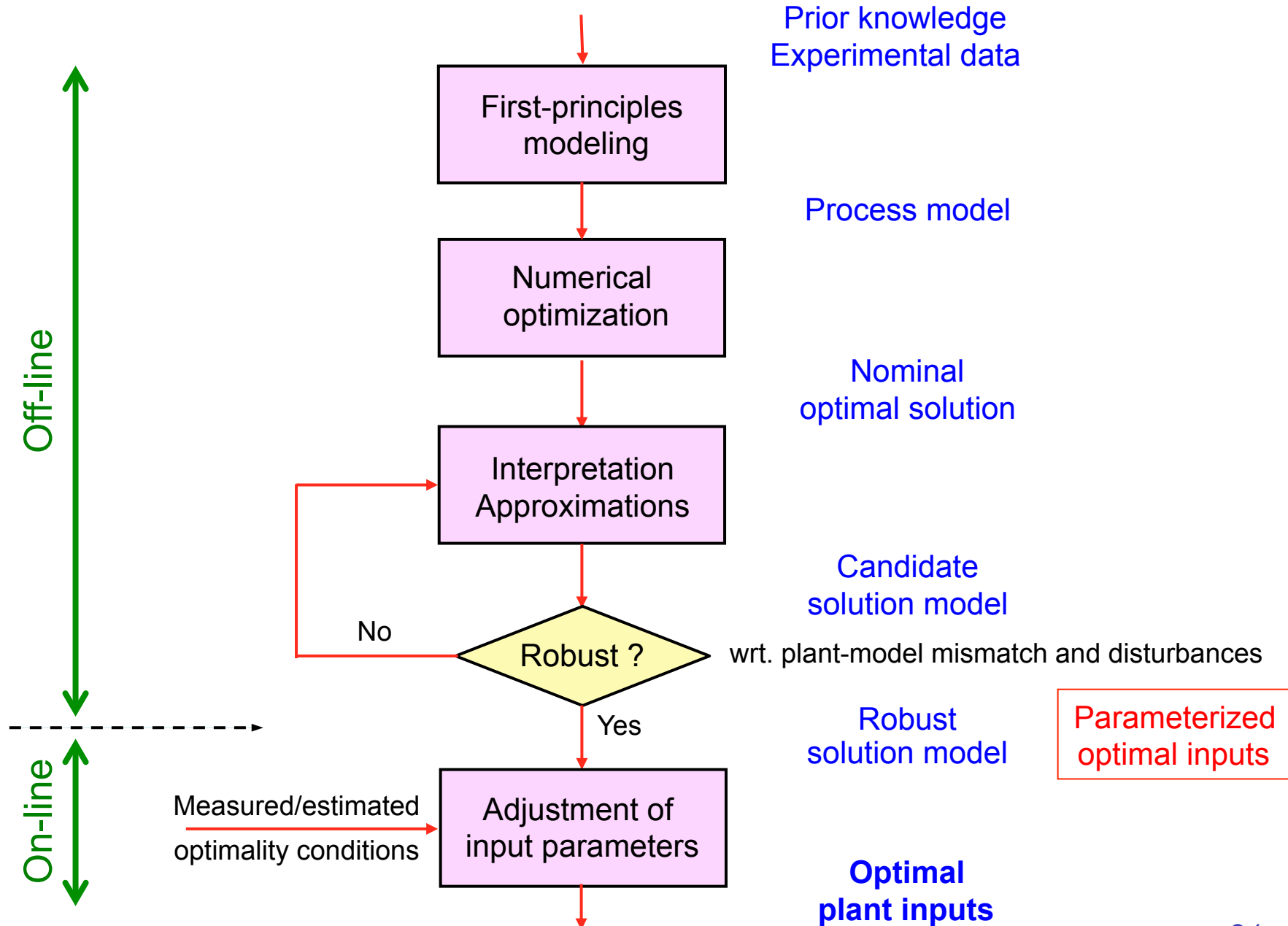
... that is structurally identical !



Parameterized optimal input

- 3 arcs: F_{engine} , v_{max} and F_{brakes}
- 2 switching times: t_1 and t_2

Generation of a Solution Model



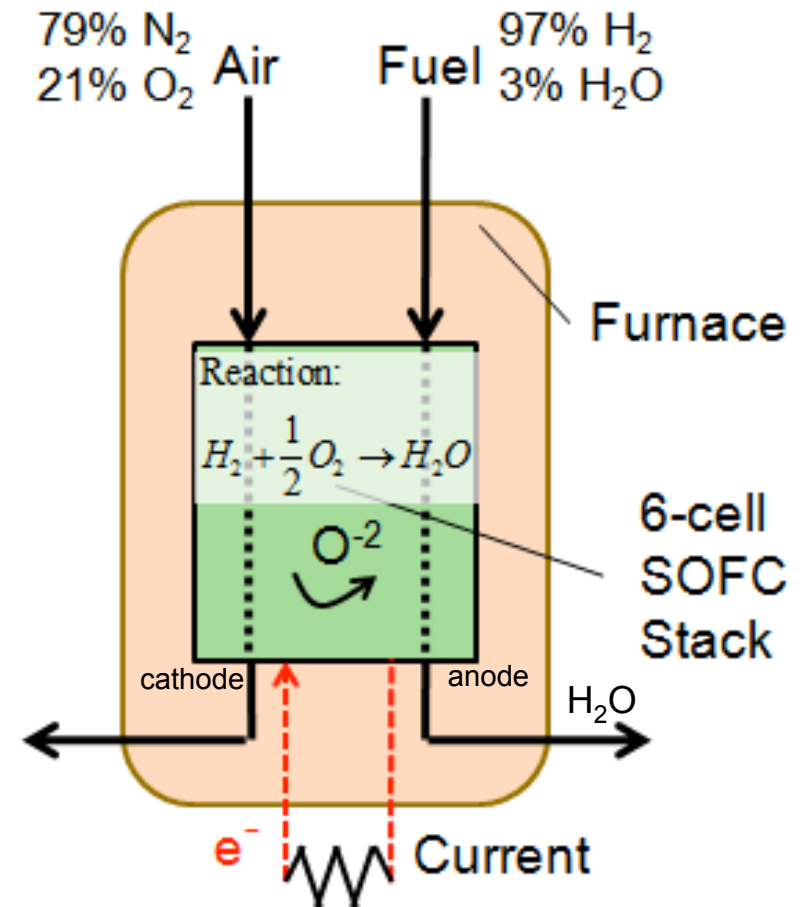
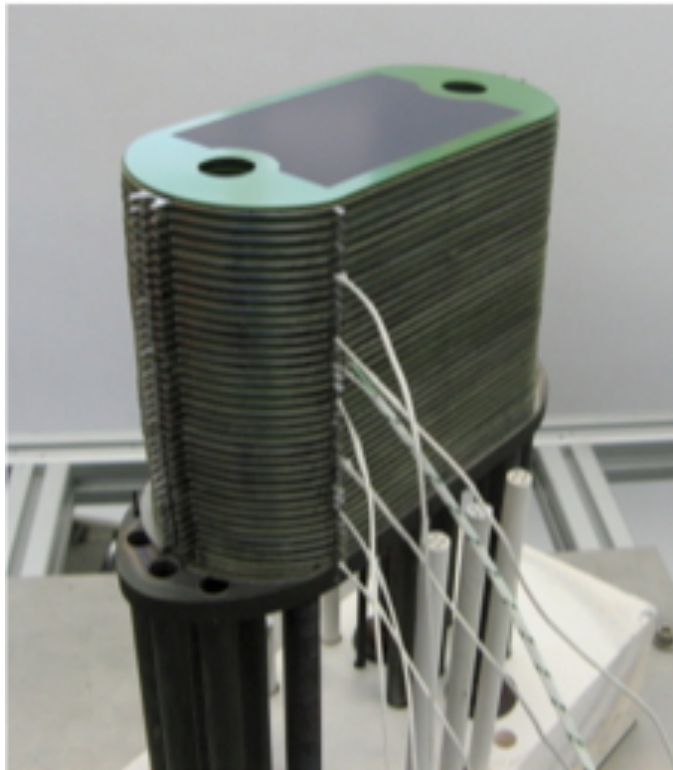
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 - Batch polymerization reactor (NCO tracking)



1. Solid Oxide Fuel Cell Stack

RTO via Modifier Adaptation © LA



- Stack of 6 cells, active area of 50 cm², metallic interconnector
- Anodes : standard nickel/yttrium stabilized-zirconia (Ni-YSZ)
- Electrolyte : dense YSZ.
- Cathodes: screen-printed (La, Sr)(Co, Fe)O₃
- Operation temperatures between 650 and 850°C.

Experimental Features

- **Objective:** maximize electrical efficiency
- Meet power demand that changes unexpectedly
- **Inputs:** flowrates of H₂ and O₂, current
- **Outputs:** power density, cell potential
- Time-scale separation
 - *slow temperature dynamics, treated as process drift !*
 - *static model (for the rest)*
- Inaccurate model in the operating region (power, cell)

Strategy for Online Optimization

Repeated Numerical Optimization

- Solve a static optimization problem every 10 sec
- Apply the optimal inputs to the stack
- Measure the resulting constraint values
- Adapt the modifiers ε to match the active constraints

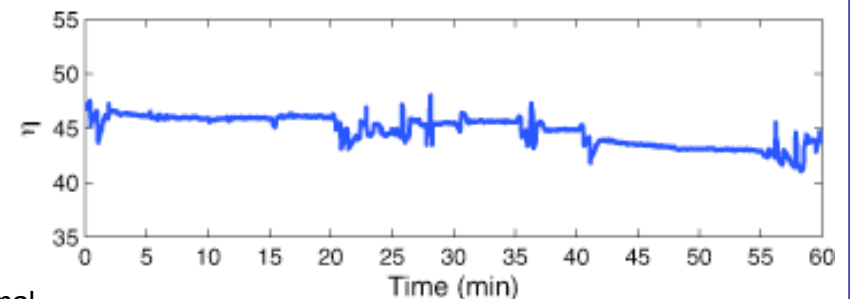
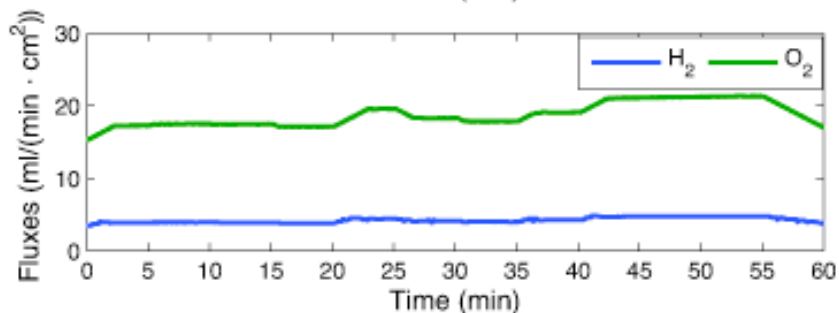
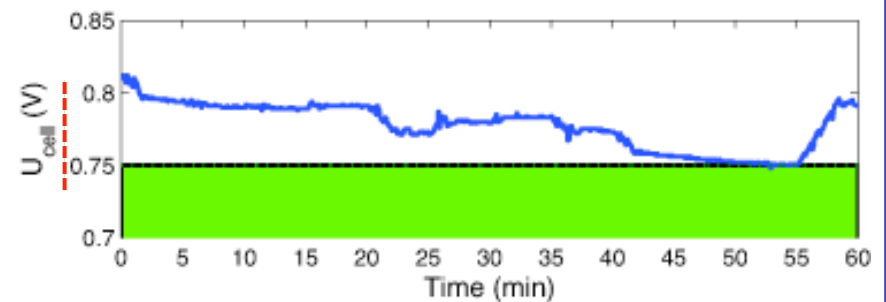
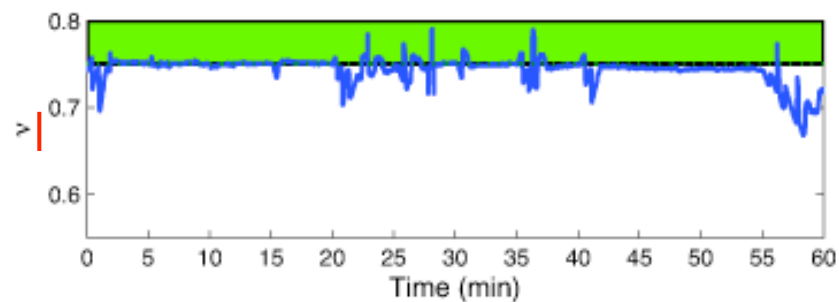
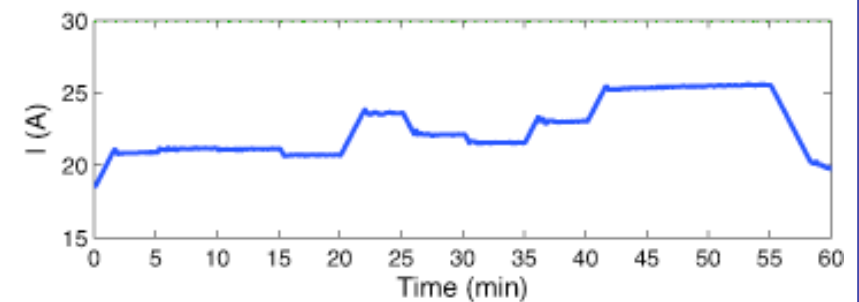
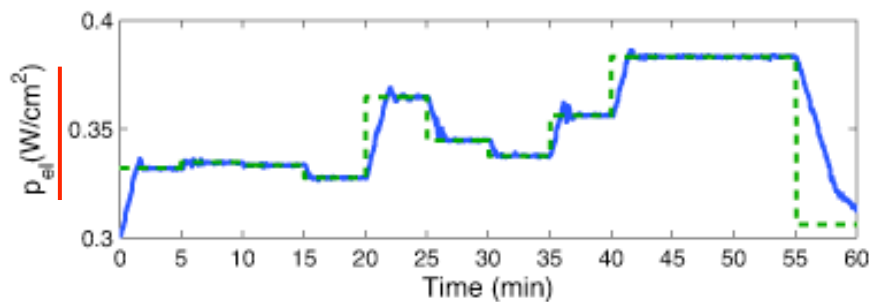
$$\begin{aligned} \max_{\mathbf{u}_k} \quad & \eta(\mathbf{u}_k, \boldsymbol{\theta}) \\ \text{s.t.} \quad & p_{el}(\mathbf{u}_k, \boldsymbol{\theta}) + \varepsilon_{k-1}^{p_{el}} = \underline{p_{el}^S} \\ & U_{cell}(\mathbf{u}_k, \boldsymbol{\theta}) + \varepsilon_{k-1}^{U_{cell}} \geq \underline{0.75 V} \quad \text{to avoid cell degradation} \\ & \nu(\mathbf{u}_k) \leq \underline{0.75} \quad \text{to avoid local fuel starvation} \\ & 4 \leq \lambda_{air}(\mathbf{u}_k) \leq 7 \quad \text{to avoid steep thermal gradients} \\ & \mathbf{u}_{1,k} \geq 3.14 \text{ mL}/(\text{min cm}^2) \\ & \mathbf{u}_{3,k} \leq 30 \text{ A} \end{aligned}$$

$$\mathbf{u}_k = \begin{bmatrix} u_{1,k} = \dot{n}_{H_2,k} \\ u_{2,k} = \dot{n}_{O_2,k} \\ u_{3,k} = I_k \end{bmatrix}$$

$$\begin{aligned} \varepsilon_k^{p_{el}} &= (1 - K_{p_{el}}) \varepsilon_{k-1}^{p_{el}} + K_{p_{el}} [p_{el,p,k} - p_{el}(\mathbf{u}_k, \boldsymbol{\theta})] \\ \varepsilon_k^{U_{cell}} &= (1 - K_{U_{cell}}) \varepsilon_{k-1}^{U_{cell}} + K_{U_{cell}} [U_{cell,p,k} - U_{cell}(\mathbf{u}_k, \boldsymbol{\theta})] \end{aligned}$$

Experimental Results

- Random power changes every 5 min
- RTO every 10 s, matches the active constraints at steady state



λ_{air} maximal

2. Optimization of Polymerization Reactor

NCO tracking © LA

■ Industrial features

- 1-ton reactor, risk of runaway
- Initiator efficiency can vary considerably
- Several recipes
 - *different initial conditions*
 - *different initiator feeding policies*
 - *use of chain transfer agent*
 - *use of reticulant*

AQUA+TECH

SPECIALTIES SA

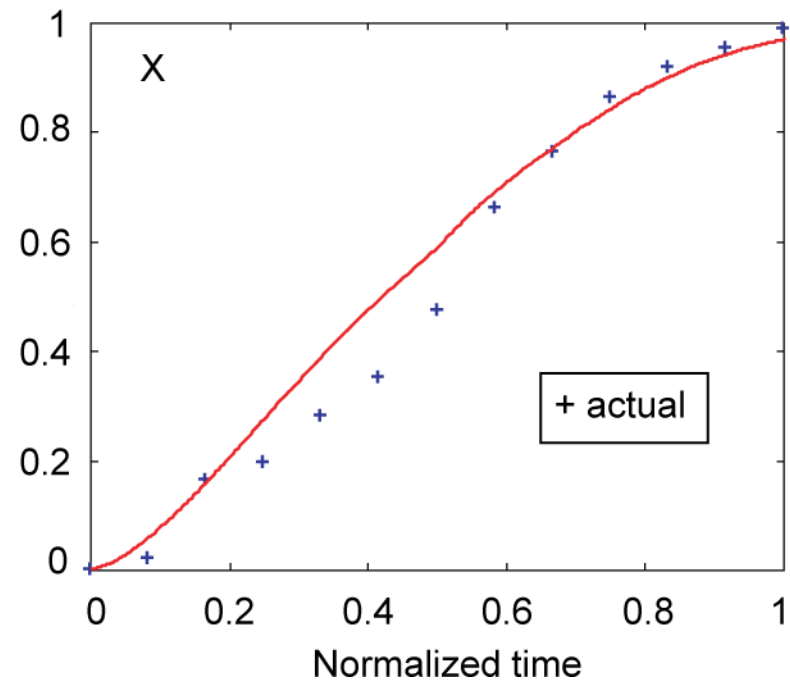
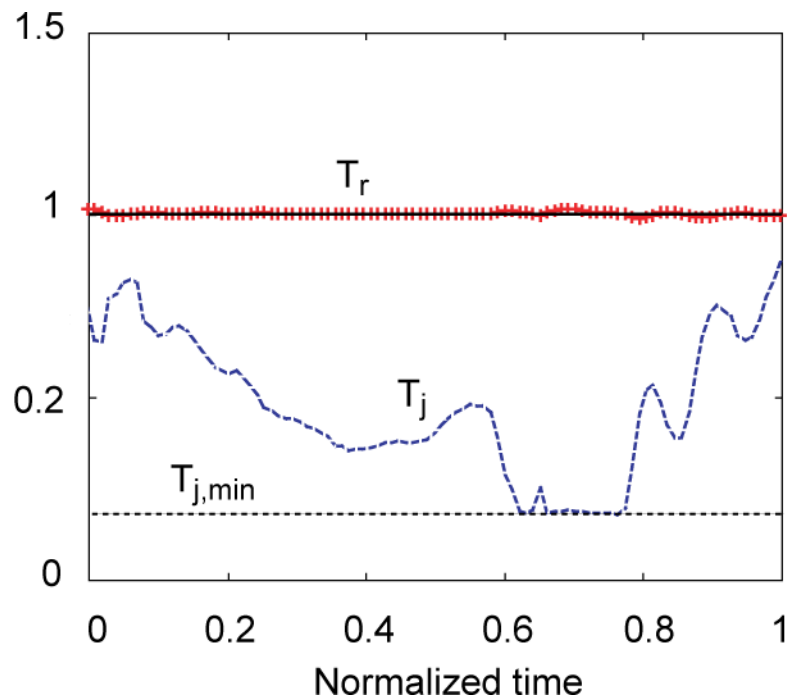


- 
- Modeling difficulties
 - Uncertainty

■ Challenge: Implement (near) optimal operation for various recipes

G. François *et al.*, Run-to-run adaptation of a semi-adiabatic policy for the optimization of an industrial batch polymerization process, *I&EC Research*, 43, 7238-7242 (2004)

Industrial Practice



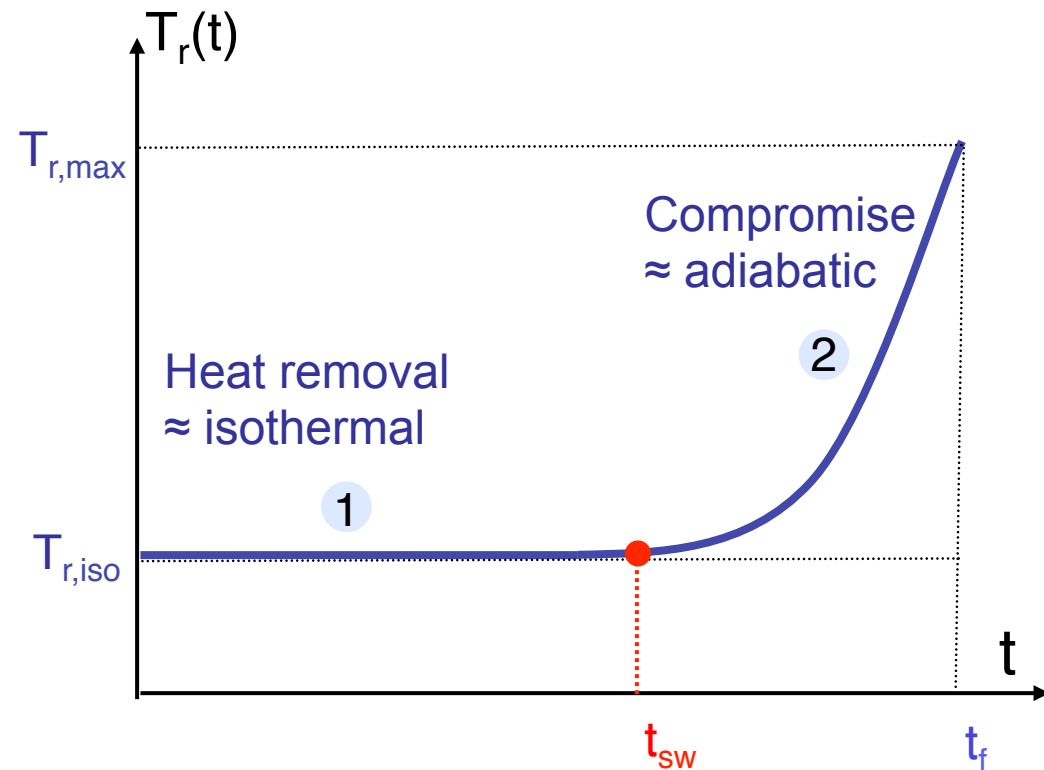
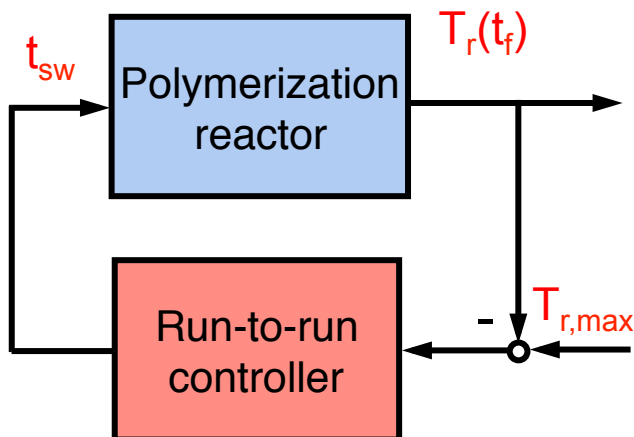
$T_r(t)$ to minimize the batch time ?

Strategy for Run-run Optimization

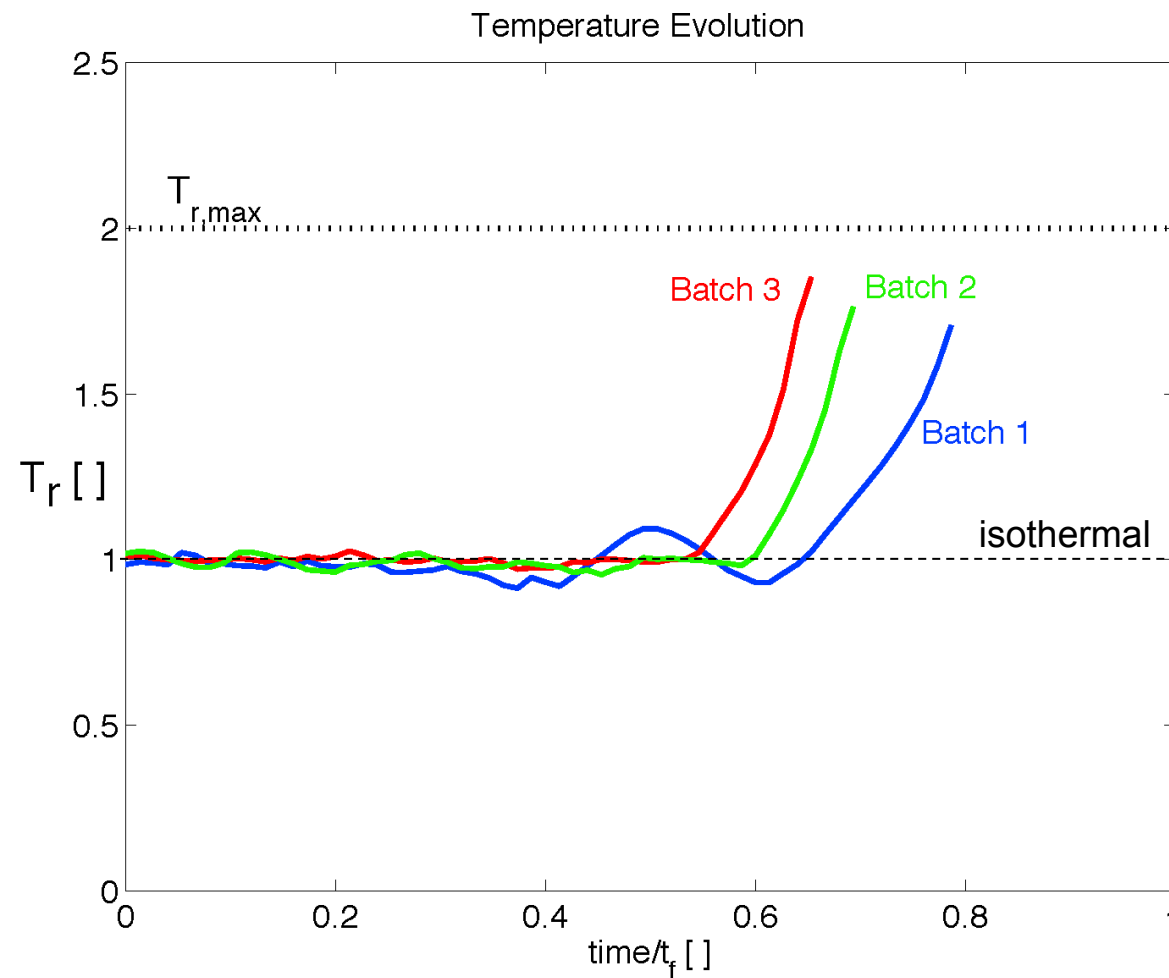
Tendency model

Optimality is linked with meeting the most restrictive constraint $T_r(t_f) = T_{r,max}$

Strategy: Manipulate t_{sw} on a run-to-run basis to force $T_r(t_f)$ at $T_{r,max}$



Industrial Results



Conclusions

- Process models are often inadequate for optimization
 - use **real-time measurements** for appropriate adaptation

- Which measurements to use? How to best exploit them?
 - **Outputs**: easily available, not necessarily appropriate → KKT elements
 - **KKT modifiers** allow meeting KKT conditions
 - modifier adaptation^{©LA} (explicit optimization)
 - NCO tracking^{©LA} (implicit optimization)

- Key challenge is **estimation of plant gradient**
 - **Use of successive operational points** → BFGS-type of scheme
 - **Dual RTO**

**Thank you
for your attention !**